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A Study of Demoulding Force Prediction Applied to Periodic Mould Surface Profiles

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A STUDY OF DEMOULDING FORCE PREDICTION APPLIED TO PERIODIC MOULD SURFACE PROFILES

The following was presented at the Society of Plastic Engineers conference, ANTEC 2010, held in Orlando, Florida from May 16-20 2010.

For further details and to access the full paper please refer to the conference proceedings.

-Kevin D. Delaney,
26May2010



A STUDY OF DEMOULDING FORCE PREDICTION APPLIED TO PERIODIC MOULD SURFACE PROFILES

K. Delaney, Dublin Institute of Technology.

Dr. G. Bissacco, University of Padova.

Dr. D. Kennedy, Dublin Institute of Technology.

Aim of this research

Can we predict demoulding forces if we know:

- Parameters used to fabricate the replication tool
- Replication process parameters
- Details of the mould and part materials

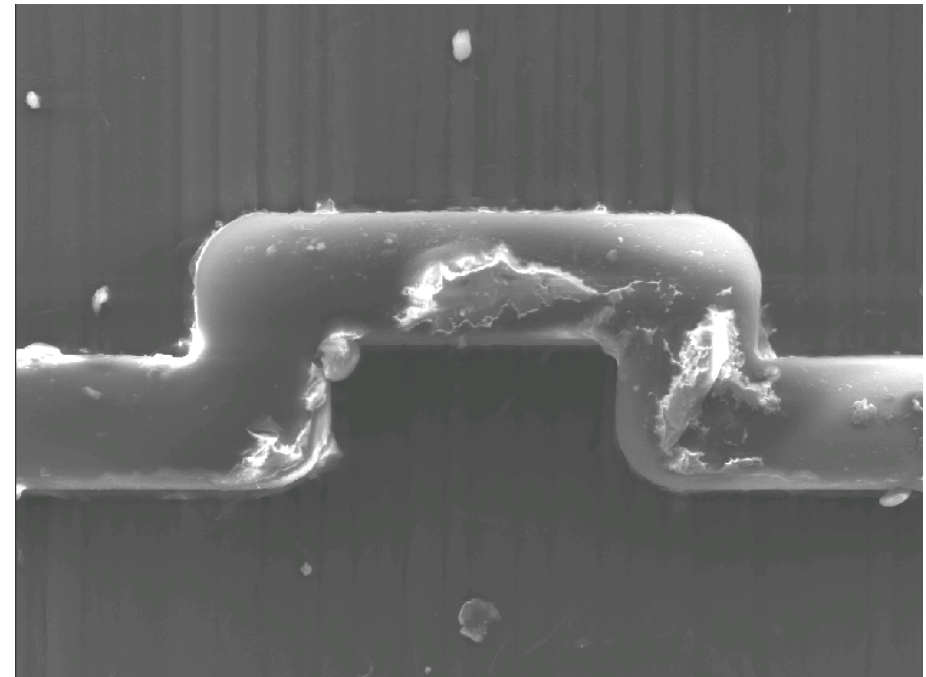
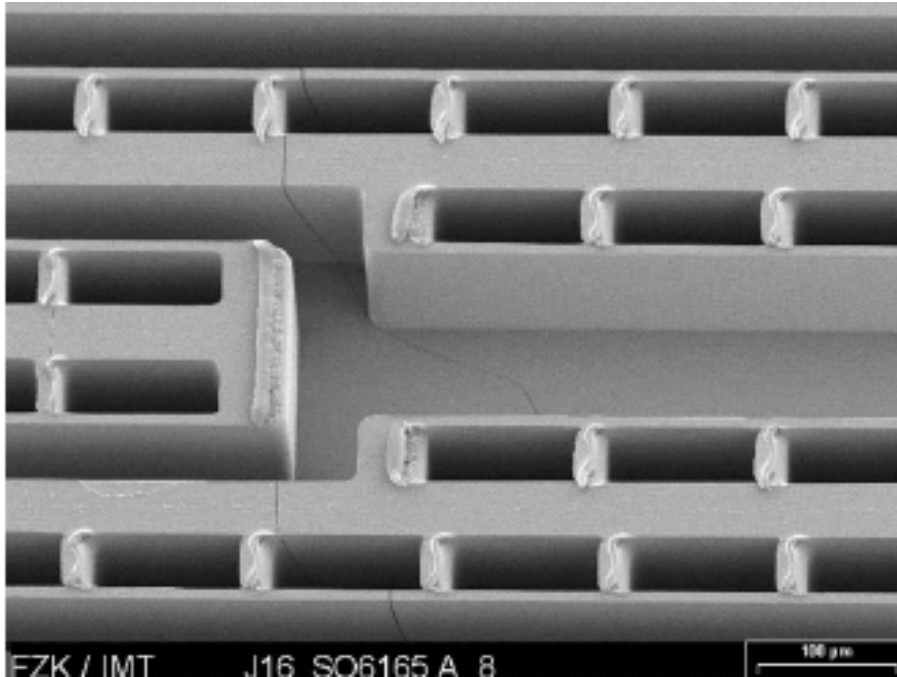


Presentation Outline

- The problem of demoulding force
- Demoulding force modeling
- Note regarding replication tool surfaces
- Adapting Colton et al model to periodic profiles
- Validation of the model

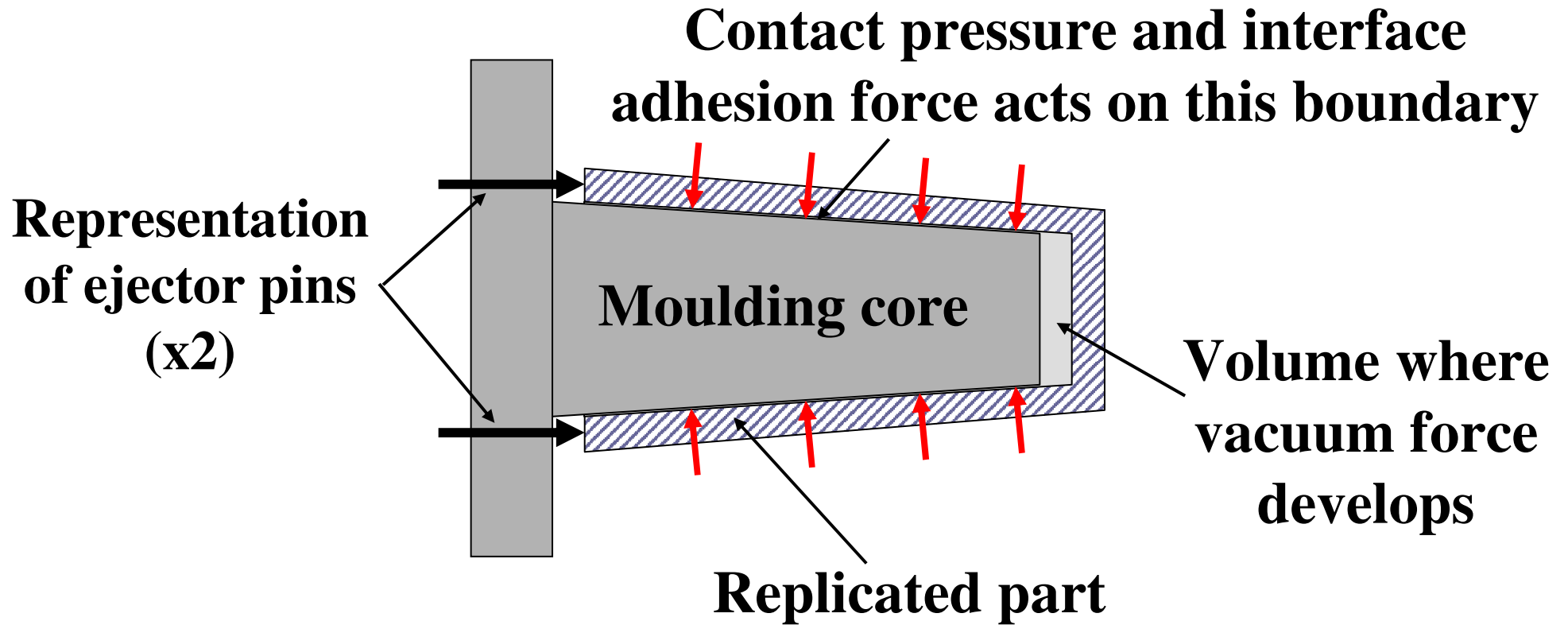


Examples of the problem at micro scale

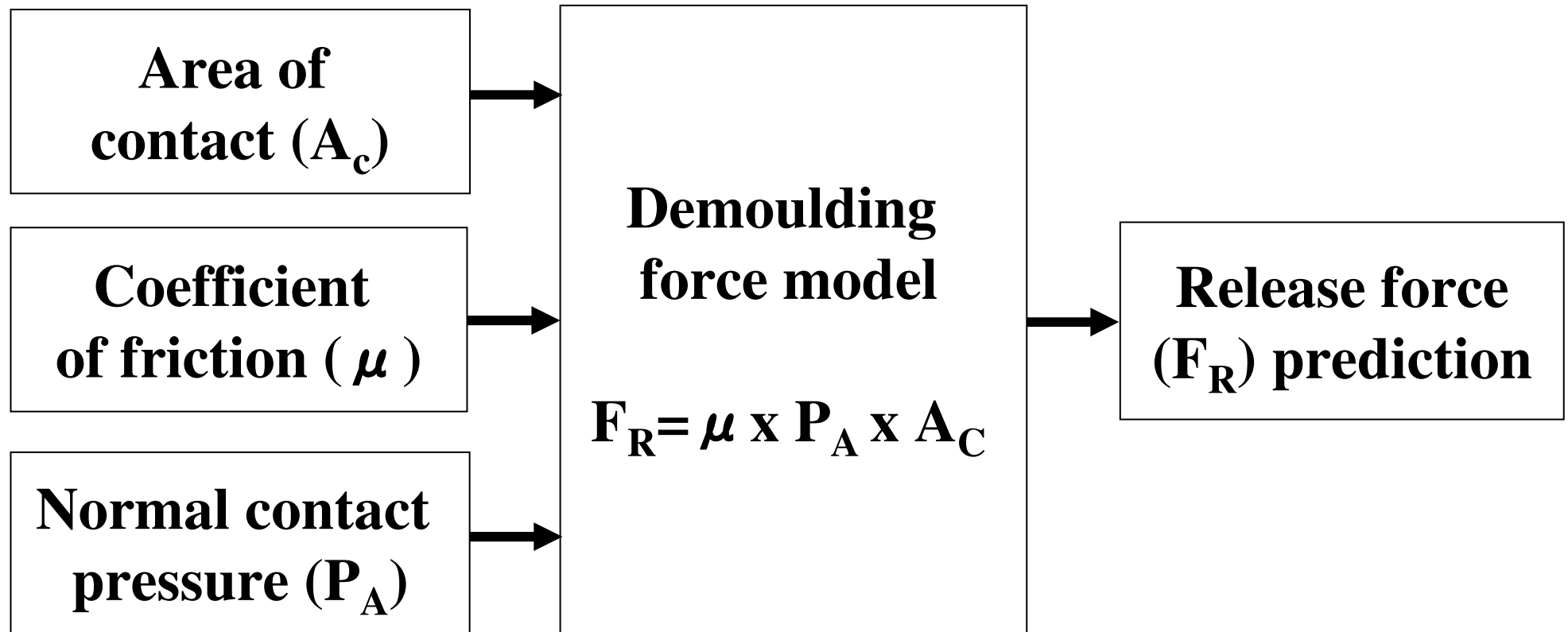


[Worgull et al]

Contributors to demoulding force

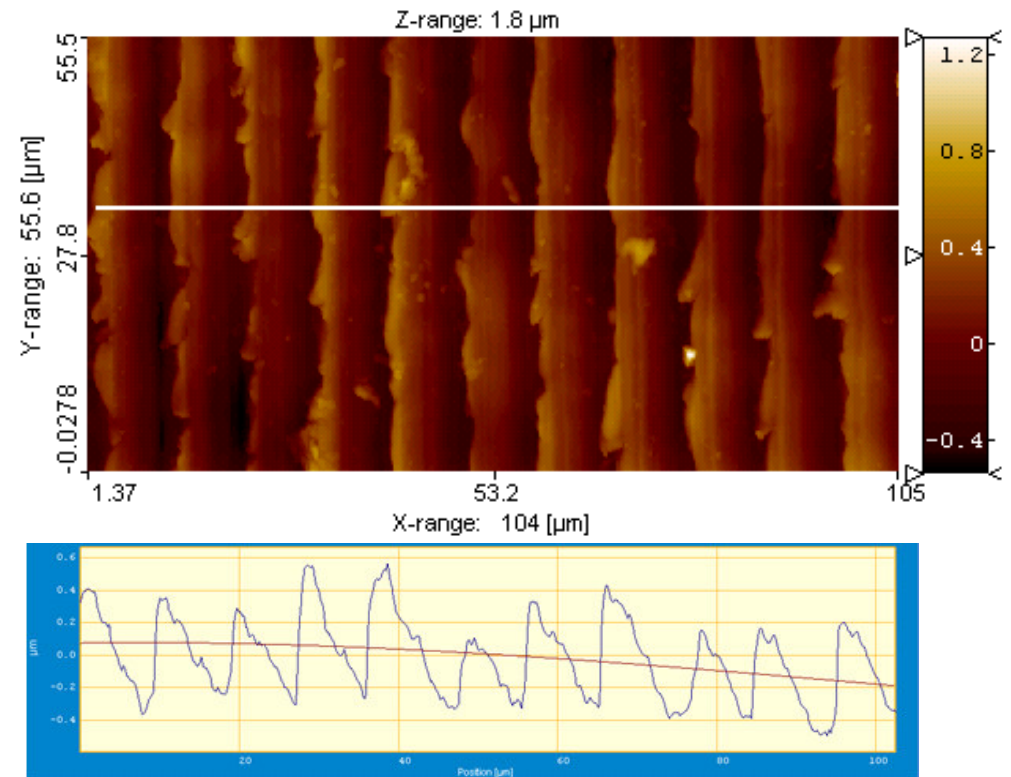


Demoulding force modelling



Note regarding replication tool surfaces

- Replication tools are mainly produced by mechanical processes with an inherent surface roughness.
- Even at the micro scale asperities and burrs cause interlocking which results in demoulding problems.
- During demoulding either the part or tool have to deform to slide over each other.

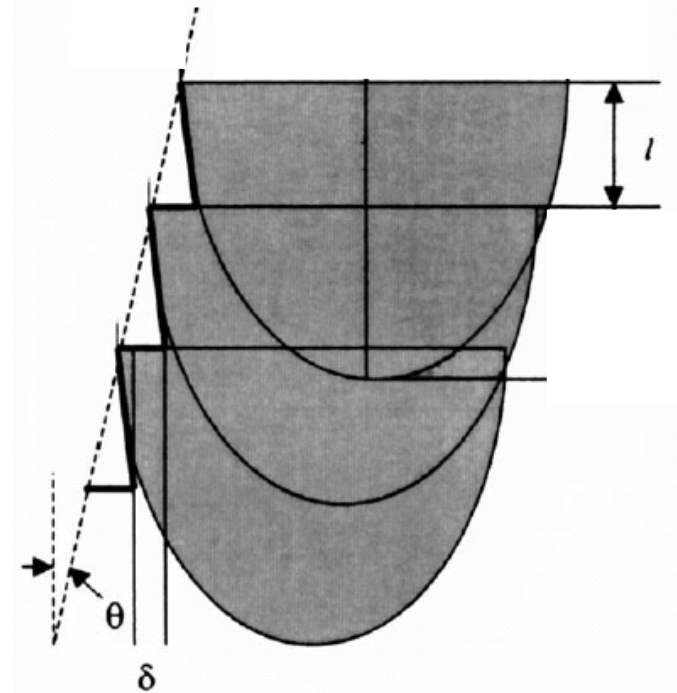


Micro replication tool and surface profile

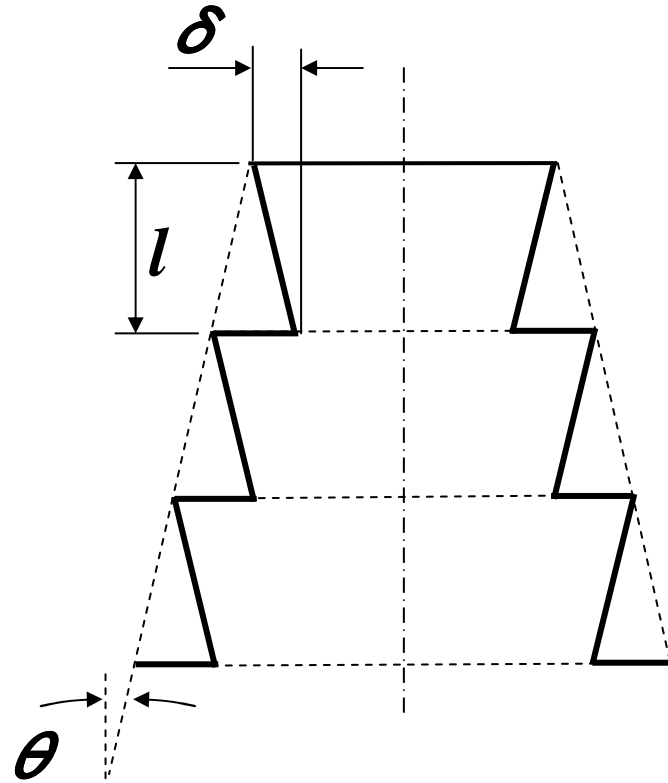
The Colton et al model - 1

- Developed for stereo-lithographic tools
- Stair-like surface profile

$$F_{ej} = F_{fric,therm} + F_{def,stair}$$

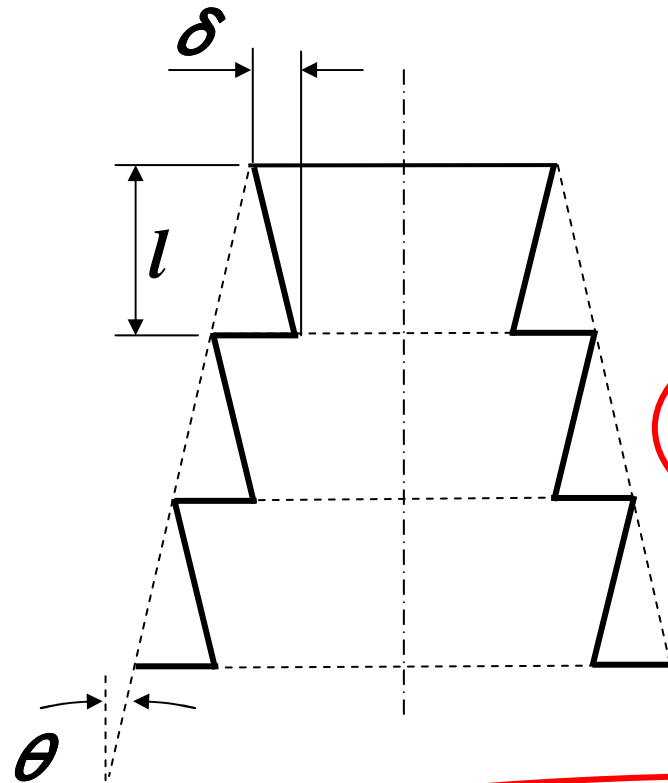


The Colton et al model - 2



$$\mu_{eq} = \mu + fn(\delta, l, \theta, Temperature, materials)$$

The Colton et al model - 2



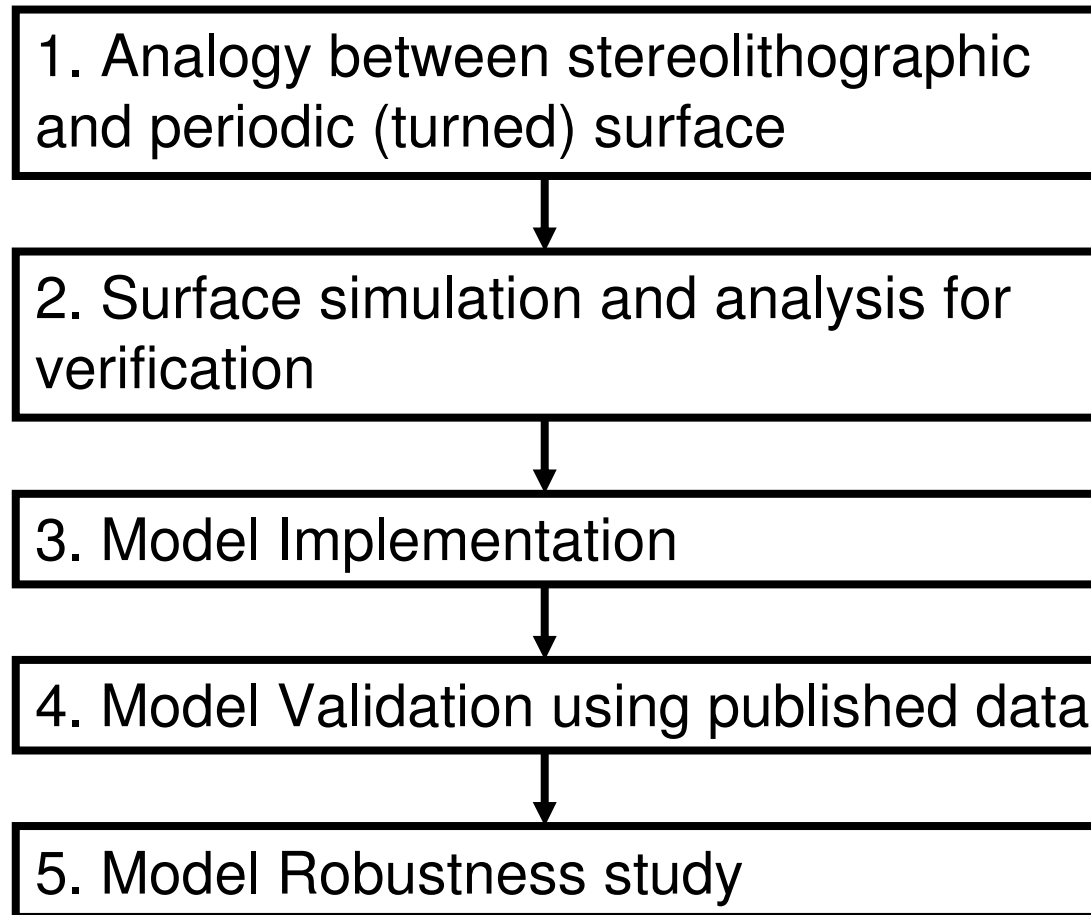
*Additional μ contribution
due to surface roughness*

$$\mu_{eq} = \mu + fn(\delta, l, \theta, Temperature, materials)$$

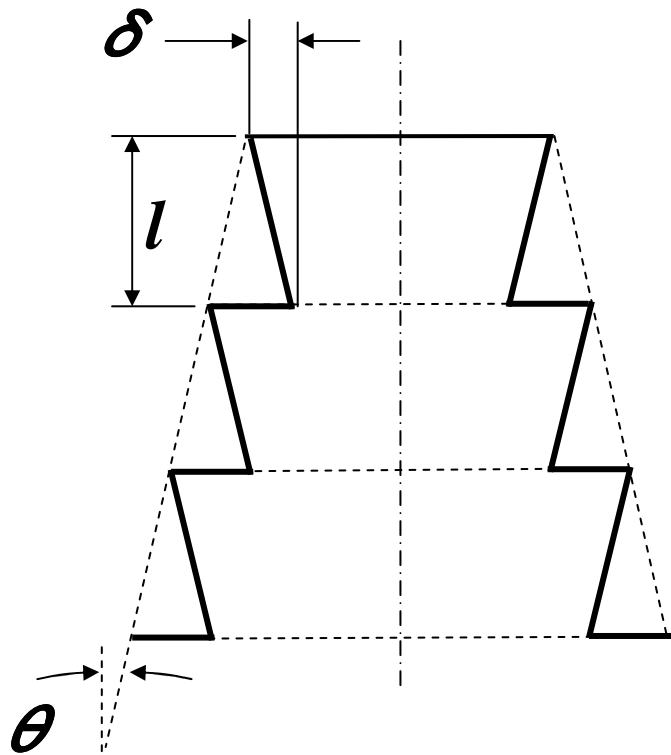
The Colton et al model - 3

- The Colton et al model has already been applied.
 - It tries to explicitly capture how the coefficient of friction varies with surface roughness.
 - We can benefit from adapting it for other periodic surfaces.
-

Adapting the Colton et al model



Analogy between stereolithographic and periodic (turned) surface - 1

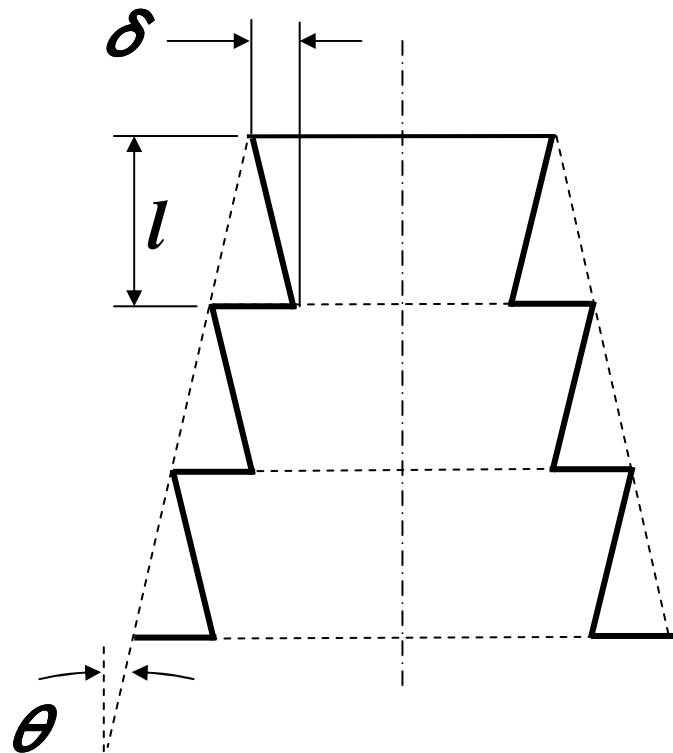


Stereolithographic,
stair-step profile

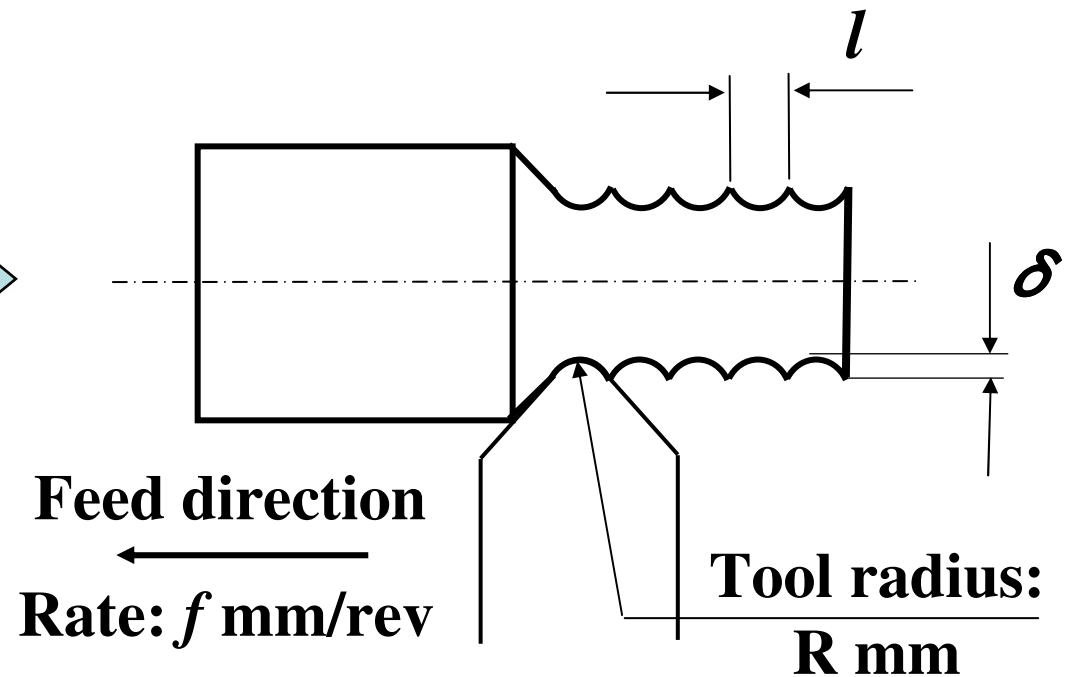


Turned periodic mould
surface profile

Analogy between stereolithographic and periodic (turned) surface - 1

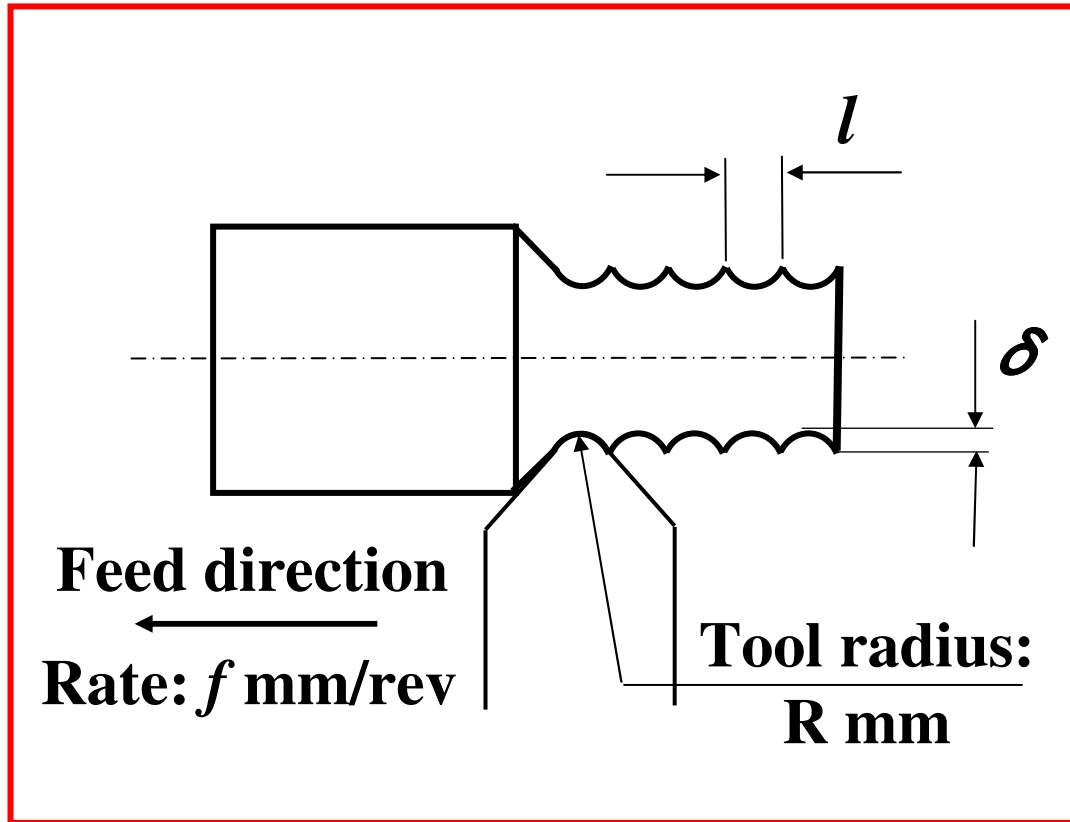


Stereolithographic,
stair-step profile



Turned periodic mould
surface profile

Analogy between stereolithographic and periodic (turned) surface - 2

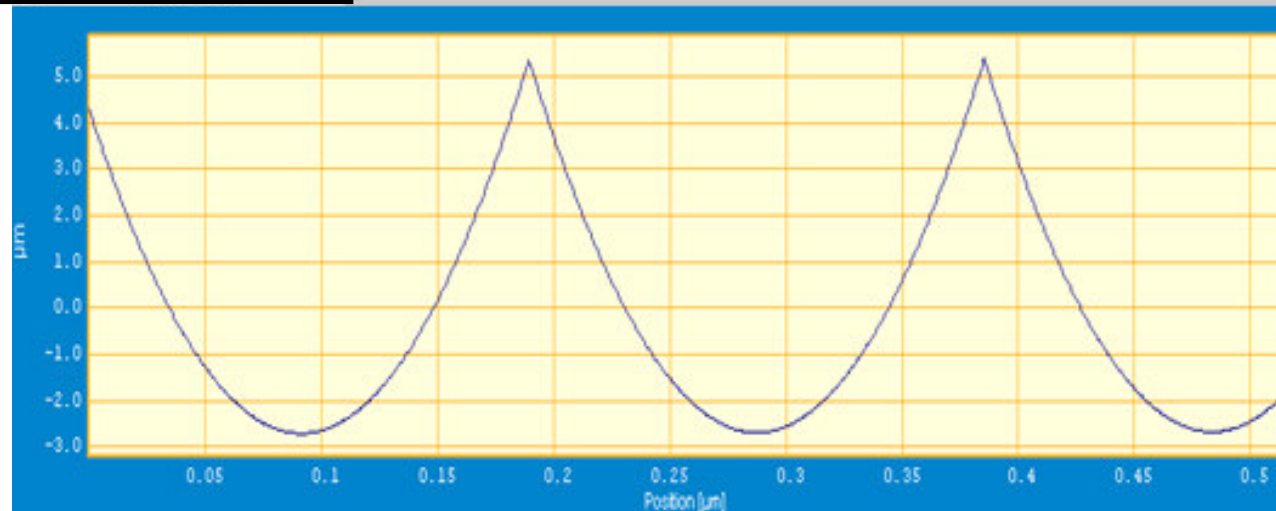
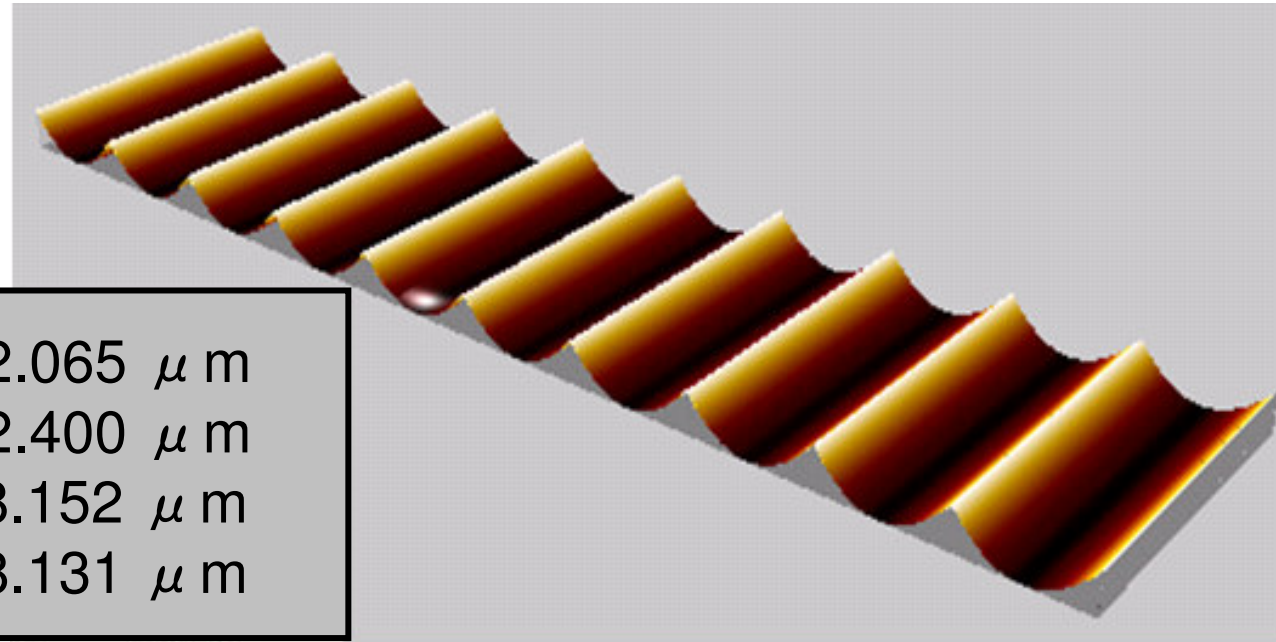


$$Ra = \frac{f^2}{32 \times R}$$

$$\delta = \frac{f^2}{8 \times R}$$

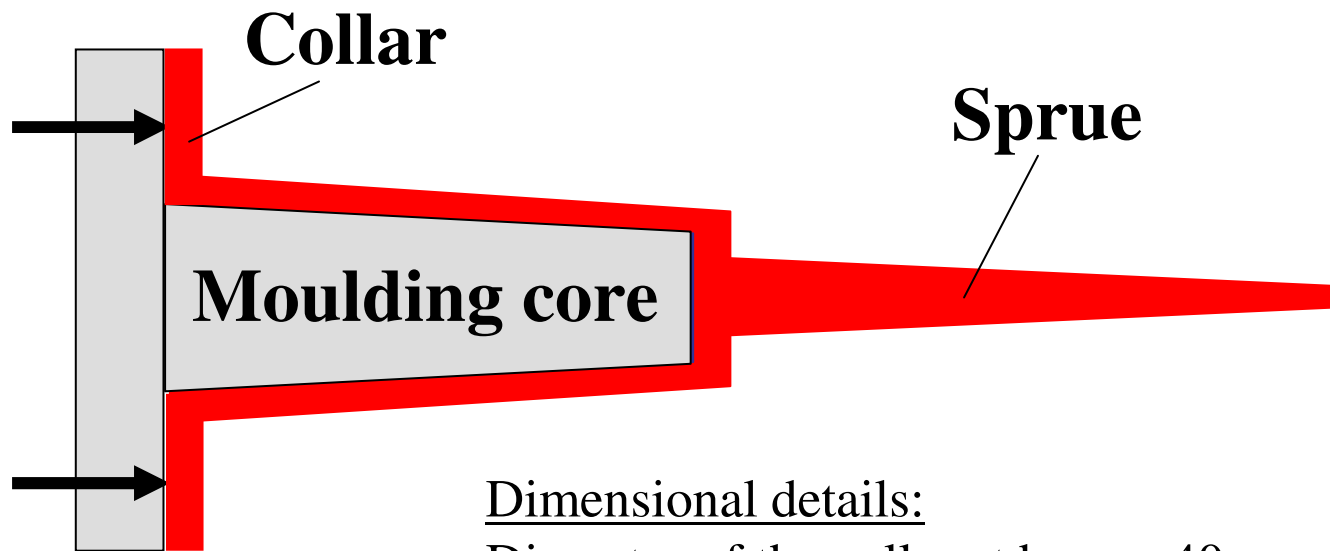
Surface simulation and analysis for verification

| | | |
|----|-------|---------------|
| Sa | 2.065 | μm |
| Sq | 2.400 | μm |
| Sy | 8.152 | μm |
| Sz | 8.131 | μm |



Model implementation

Details of Hopkinson and Dickens component used for validation



Dimensional details:

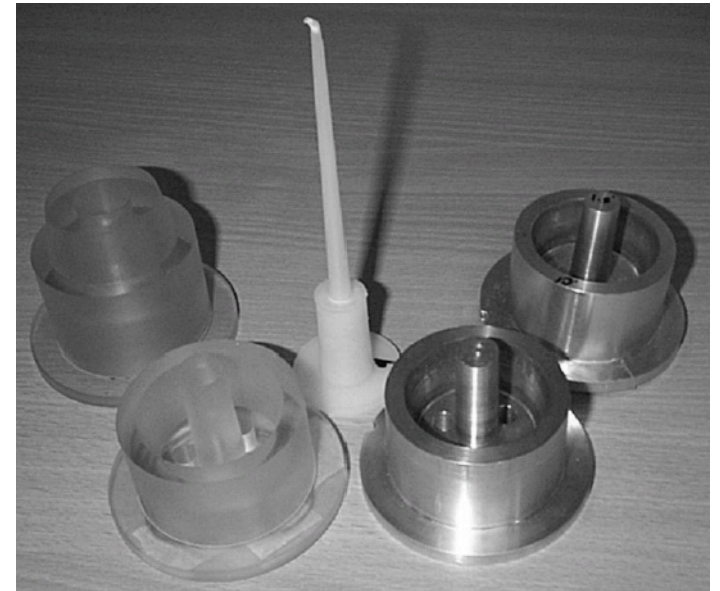
Diameter of the collar at base = 40mm,

Diameter at opening of collar = 16mm,

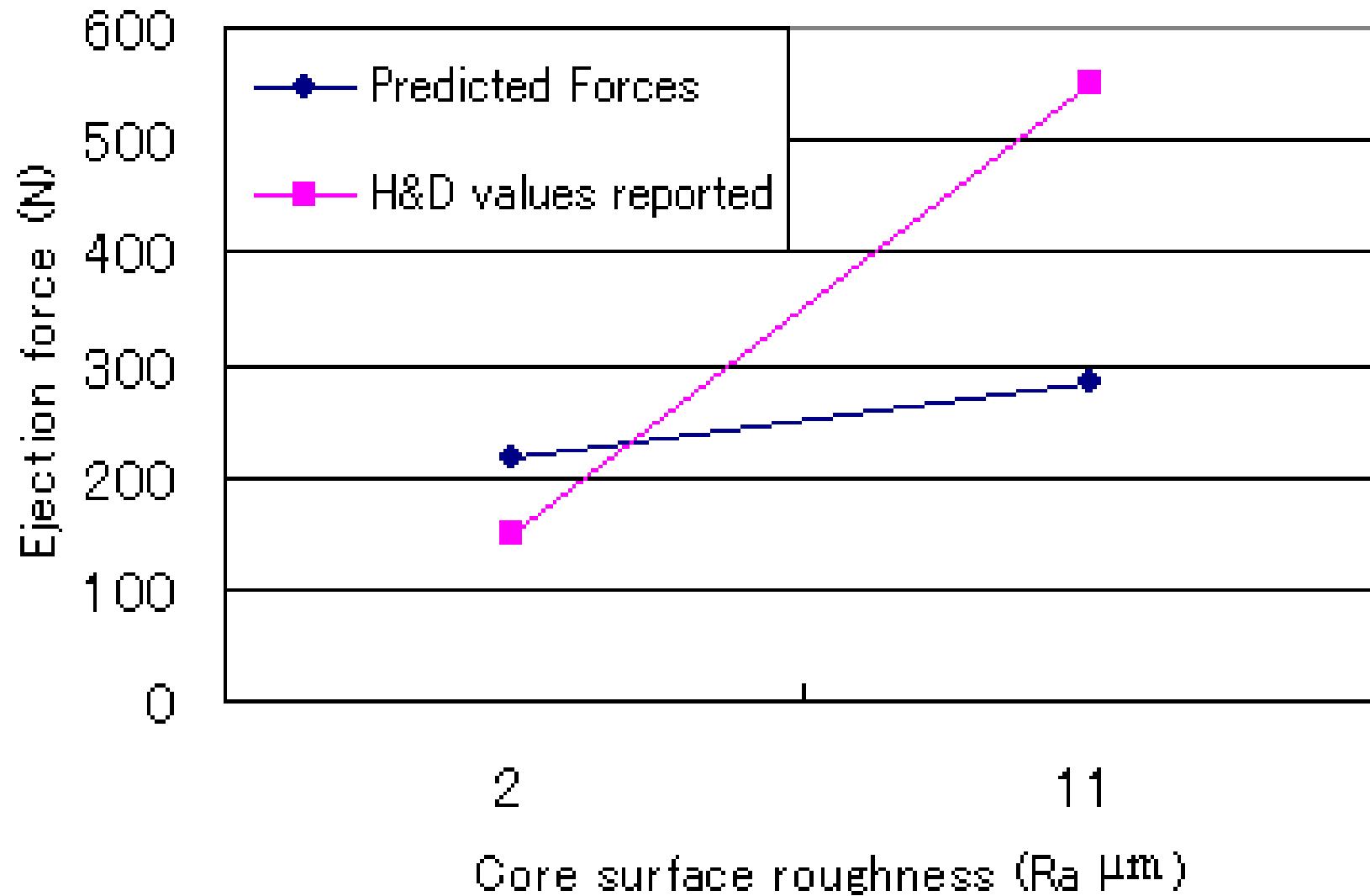
Length of the moulding = 40mm,

All walls 2mm thick,

Draft on male feature = 1.5 degrees.



Model validation



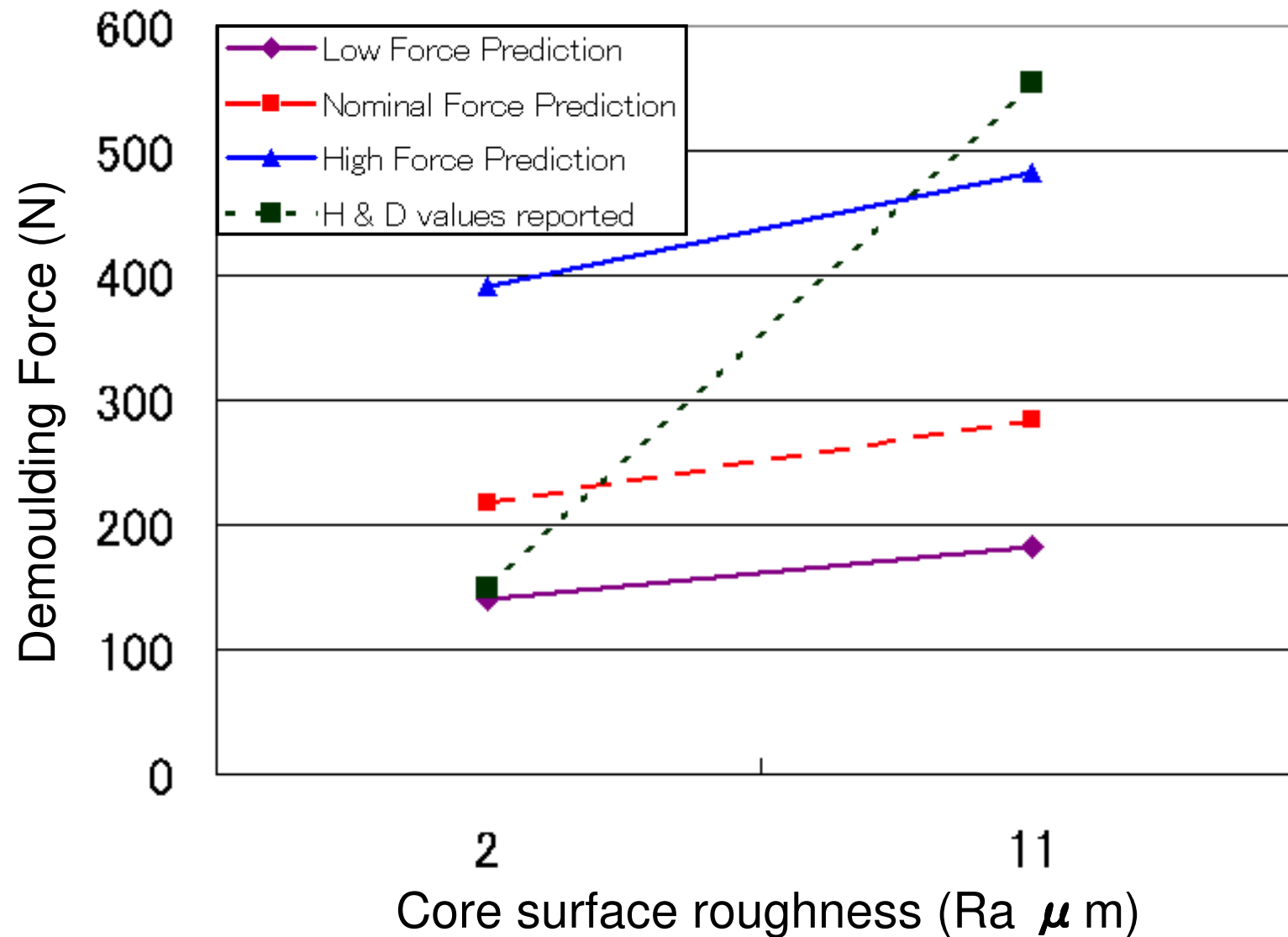
Robustness of the Colton et al Model - 1

| Parameter | | Value |
|--------------------------------------|-----------------|------------|
| Cutting tool radius (mm) | R | 0.2 ~ 1.0 |
| Mould temperature at ejection (° C) | T _{me} | 30 ~ 60 |
| Mould temperature at injection (° C) | T _{mi} | 15 ~ 49 |
| Component ejection temperature (° C) | T _{pe} | 40 ~ 60 |
| Polymer melting temperature (° C) | T _{pm} | 160 ~ 173 |
| Coefficient of friction | μ | 0.25 ~ 0.4 |

Robustness of the Colton et al Model - 1

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Robustness of the Colton et al Model - 2



Conclusion

- Limitations of the Colton et al model applied to periodic (non stereo-lithographic) surfaces highlighted.
 - Some issues related to micro machined surfaces listed.
 - More advanced model needed
 - Should consider viscoelastic behaviour of replicating material together with any permanent deformation (instead of assuming elastic deformation).
 - Model should be suitable for implementation in a Finite Element Modelling package.
 - Efforts are ongoing towards the development of such a model.
-

Questions?



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